

S14	5	704	3✓	0.025	-	0.025	✓	100.00%	0.025
S14	5	705	3✓	0.016	-	0.014	-	87.50%	0.016
S14	5	706	3✓	0.023	✓	0.022	-	95.65%	0.023
S14	5	707	3✓	0.064	✓	0.065	✓	101.56%	0.064
S14	5	708	3✓			0.036	✓		0.042
S14	5	709	3✓			0.063	✓		0.081
S14	5	710	3✓	0.070	-	0.069	-	98.57%	0.070
S14	5	711	3✓			0.073	✓		0.094
S14	5	712	3✓			0.047	✓		0.055
S14	5	713	3✓	0.105	-	0.104	-	99.05%	0.105
S14	5	714	3✓			0.062	✓		0.080
S14	5	715	3✓	0.022	-	0.016	-	72.73%	0.022
S14	5	716	3✓	0.028	-	0.029	-	103.57%	0.028
S14	5	717	3✓	0.042	-	0.037	-	88.10%	0.042
S14	5	718	3✓	0.021	-	0.017	-	80.95%	0.021
S14	5	801	3✓	0.029	-	0.030	-	103.45%	0.029
S14	5	802	3✓	0.013	-	0.011	-	84.62%	0.013
S14	5	803	3✓			0.013	✓		0.014
S14	5	804	3✓			0.011	✓		0.012
S14	5	805	3✓	0.017	-	0.017	✓	100.00%	0.017
S14	5	806	3✓	0.042	-	0.045	✓	107.14%	0.042
S14	5	807	3✓	0.020	-	0.020	-	100.00%	0.020
S14	5	808	3✓	0.022	-	0.023	✓	104.55%	0.022
S14	5	809	3✓	0.069	-	0.070	✓	101.45%	0.069
S14	5	810	3✓			0.033	✓		0.039
S14	5	811	3✓	0.033	-	0.031	-	93.94%	0.033
S14	5	812	3✓			0.039	✓		0.046
S14	5	813	3✓			0.041	✓		0.048
S14	5	814	3✓	0.028	-	0.026	-	92.86%	0.028
S14	5	815	3✓	0.014	-	0.011	-	78.57%	0.014
S14	5	816	3✓			0.010	-		0.011
S14	5	817	3✓	0.020	-	0.019	-	95.00%	0.020
S14	5	818	3✓			0.010	-		0.011

MEAN	0.044	0.022	82.79%	0.027
------	-------	-------	--------	-------

S-14-5 ✓ CORRECT Bat Not Complete
~~NEED~~ Last fires
 NEED Ratios
 4-27-90

S14	5	1	3	0.016	0.015	93.75%
S14	5	2	3	0.015	0.013	86.67%
S14	5	3	3	0.034	0.027	79.41%
S14	5	4	3	0.085	0.068	80.00%
S14	5	5	3	0.170	0.124	72.94%
S14	5	6	3	0.071	0.050	70.42%
S14	5	7	3	0.140	0.100	71.43%
S14	5	8	2	0.321	0.100	31.15%
S14	5	9	1	0.107	0.063	58.88%
S14	5	10	1	0.052	0.022	42.31%
S14	5	11	2	0.042	0.036	85.71%
S14	5	12	3	0.047	0.045	95.74%
S14	5	13	3	0.008	0.009	112.50%
S14	5	14	3		0.015	ERR
S14	5	15	3		0.006	ERR
S14	5	16	3	0.020	0.019	95.00%
S14	5	17	3		0.011	ERR
S14	5	21	3		0.031	ERR
S14	5	22	2	0.036	0.033	91.67%
S14	5	23	3	0.035	0.032	91.43%
S14	5	24	3		0.046	ERR
S14	5	25	3	0.100	0.091	91.00%
S14	5	26	3	0.057	0.051	89.47%
S14	5	27	3	0.158	0.145	91.77%
S14	5	28	1	0.045	0.031	68.89%
S14	5	29	1	0.022	0.022	100.00%
S14	5	30	1	0.053	0.042	79.25%
S14	5	31	1	0.033	0.029	87.88%
S14	5	32	2	0.017	0.018	105.88%
S14	5	33	3	0.011	0.009	81.82%
S14	5	34	2		0.008	ERR
S14	5	35	2		0.010	ERR
S14	5	36	2		0.008	ERR
S14	5	37	2		0.007	ERR
S14	5	41	3	0.028	0.027	96.43%
S14	5	42	3	0.040	0.038	95.00%
S14	5	43	3	0.078	0.058	74.36%
S14	5	44	3	0.046	0.041	89.13%
S14	5	45	3	0.082	0.072	87.80%
S14	5	46	2	0.056	0.046	82.14%
S14	5	47	3		0.036	ERR
S14	5	48	2	0.028	0.017	60.71%
S14	5	49	3		0.015	ERR
S14	5	50	3		0.015	ERR
S14	5	51	2		0.011	ERR
S14	5	52	2	0.016	0.012	75.00%
S14	5	53	2		0.007	ERR
S14	5	54	2	0.016	0.015	93.75%
S14	5	55	2		0.007	ERR
S14	5	56	2		0.005	ERR
S14	5	57	1		0.003	ERR
S14	5	61	3		0.017	ERR
S14	5	62	3	0.024	0.022	91.67%
S14	5	63	3		0.033	ERR
S14	5	64	3		0.033	ERR
S14	5	65	3	0.043	0.024	55.81%

814	5	66	3	0.049	0.045	91.84%
814	5	67	2	0.026	0.017	65.38%
814	5	68	3		0.017	ERR
814	5	69	3		0.024	ERR
814	5	70	2	0.026	0.023	88.46%
814	5	71	1	0.017	0.008	47.06%
814	5	72	2		0.027	ERR
814	5	73	3		0.014	ERR
814	5	74	3		0.037	ERR
814	5	75	2		0.009	ERR
814	5	76	2		0.005	ERR
814	5	81	3	0.011	0.011	100.00%
814	5	82	3		0.032	ERR
814	5	83	3		0.030	ERR
814	5	84	3		0.035	ERR
814	5	85	3		0.029	ERR
814	5	86	3		0.034	ERR
814	5	87	3		0.013	ERR
814	5	88	2		0.006	ERR
814	5	89	1		0.010	ERR
814	5	90	1		0.006	ERR
814	5	91	1		0.005	ERR
814	5	92	1		0.003	ERR
814	5	93	2		0.003	ERR
814	5	94	3		0.012	ERR
814	5	95	3		0.014	ERR
814	5	96	2		0.005	ERR
814	5	101	3		0.021	ERR
814	5	102	3		0.031	ERR
814	5	103	3		0.023	ERR
814	5	104	3		0.034	ERR
814	5	105	3		0.048	ERR
814	5	106	3		0.032	ERR
814	5	107	3		0.014	ERR
814	5	108	3		0.002	ERR
814	5	109	2		0.007	ERR
814	5	110	2		0.006	ERR
814	5	111	1		0.004	ERR
814	5	112	2		0.003	ERR
814	5	113	2		0.002	ERR
814	5	114	2		0.005	ERR
814	5	115	2		0.026	ERR
814	5	121	3		0.037	ERR
814	5	122	3		0.054	ERR
814	5	123	3		0.063	ERR
814	5	124	3		0.037	ERR
814	5	125	3		0.014	ERR
814	5	126	3		0.012	ERR
814	5	127	3		0.011	ERR
814	5	128	2		0.002	ERR
814	5	129	3		0.006	ERR
814	5	130	1		0.004	ERR
814	5	131	1		0.005	ERR
814	5	132	2		0.003	ERR
814	5	133	2		0.007	ERR
814	5	134	2		0.004	ERR

S14	5	135	2		0.006	ERR
S14	5	141	3		0.058	ERR
S14	5	142	3		0.124	ERR
S14	5	143	3		0.156	ERR
S14	5	144	3		0.044	ERR
S14	5	145	3		0.035	ERR
S14	5	146	3		0.014	ERR
S14	5	147	3		0.015	ERR
S14	5	148	3		0.009	ERR
S14	5	149	3		0.008	ERR
S14	5	150	3		0.005	ERR
S14	5	151	1		0.006	ERR
S14	5	152	1		0.005	ERR
S14	5	153	3		0.006	ERR
S14	5	154	2		0.004	ERR
S14	5	161	3	0.036	0.033	91.67%
S14	5	162	3	0.107	0.101	94.39%
S14	5	163	3	0.012	0.011	91.67%
S14	5	164	3	0.129	0.099	76.74%
S14	5	165	3	0.032	0.029	90.63%
S14	5	166	3	0.013	0.010	76.92%
S14	5	167	3		0.005	ERR
S14	5	168	3		0.004	ERR
S14	5	169	3		0.003	ERR
S14	5	170	3		0.004	ERR
S14	5	171	2		0.004	ERR
S14	5	172	2	0.005	0.003	60.00%
S14	5	173	3		0.003	ERR
S14	5	181	3	0.075	0.077	102.67%
S14	5	182	3	0.190	0.159	83.68%
S14	5	183	3	0.019	0.017	89.47%
S14	5	184	3	0.065	0.062	95.38%
S14	5	185	3	0.023	0.021	91.30%
S14	5	186	3	0.010	0.007	70.00%
S14	5	187	3		0.009	ERR
S14	5	188	3		0.009	ERR
S14	5	189	3		0.005	ERR
S14	5	190	3		0.005	ERR
S14	5	191	2		0.005	ERR
S14	5	201	3	0.048	0.047	97.92%
S14	5	202	3	0.027	0.023	85.19%
S14	5	203	3	0.013	0.010	76.92%
S14	5	204	3		0.007	ERR
S14	5	205	3	0.102	0.080	78.43%
S14	5	206	3	0.027	0.024	88.89%
S14	5	207	3	0.010	0.007	70.00%
S14	5	208	2		0.002	ERR
S14	5	209	2		0.003	ERR
S14	5	210	2		0.006	ERR
S14	5	221	2		0.047	ERR
S14	5	222	3		0.028	ERR
S14	5	223	3		0.040	ERR
S14	5	224	2		0.010	ERR
S14	5	225	3		0.008	ERR
S14	5	226	2		0.005	ERR
S14	5	227	3		0.004	ERR

S14	5	228	2		0.001	ERR
S14	5	241	3		0.033	ERR
S14	5	242	3		0.034	ERR
S14	5	243	3		0.022	ERR
S14	5	244	3		0.027	ERR
S14	5	245	3		0.027	ERR
S14	5	246	3		0.006	ERR
S14	5	261	3		0.038	ERR
S14	5	262	3		0.024	ERR
S14	5	263	3		0.009	ERR
S14	5	264	2		0.006	ERR
S14	5	265	2		0.008	ERR
S14	5	281	3		0.013	ERR
S14	5	282	3		0.042	ERR
S14	5	283	3		0.006	ERR
S14	5	301	3		0.013	ERR
S14	5	302	3		0.016	ERR
S14	5	321	3		0.015	ERR
S14	5	341	3		0.017	ERR
S14	5	500	1		0.004	ERR
S14	5	501	1		0.006	ERR
S14	5	502	2		0.006	ERR
S14	5	503	3		0.010	ERR
S14	5	504	2		0.003	ERR
S14	5	505	2		0.004	ERR
S14	5	506	2	0.006	0.006	100.00%
S14	5	507	2	0.031	0.026	83.87%
S14	5	508	2	0.004	0.003	75.00%
S14	5	509	1		0.001	ERR
S14	5	510	1		0.001	ERR
S14	5	511	1		0.000	ERR
S14	5	512	1		0.003	ERR
S14	5	513	1		0.002	ERR
S14	5	514	2		0.003	ERR
S14	5	515	3		0.005	ERR
S14	5	516	3		0.007	ERR
S14	5	517	2	0.005	0.004	80.00%
S14	5	518	1		0.006	ERR
S14	5	519	2		0.003	ERR
S14	5	520	2		0.004	ERR
S14	5	521	3		0.005	ERR
S14	5	522	2		0.004	ERR
S14	5	523	3		0.005	ERR
S14	5	524	2		0.006	ERR
S14	5	525	3		0.003	ERR
S14	5	526	3		0.006	ERR
S14	5	527	3	0.011	0.012	109.09%
S14	5	528	3		0.005	ERR
S14	5	529	3	0.002	0.002	100.00%
S14	5	530	1		0.001	ERR
S14	5	531	2		0.003	ERR
S14	5	532	2		0.003	ERR
S14	5	601	3		0.015	ERR
S14	5	602	3		0.025	ERR
S14	5	603	3		0.013	ERR
S14	5	604	3		0.027	ERR

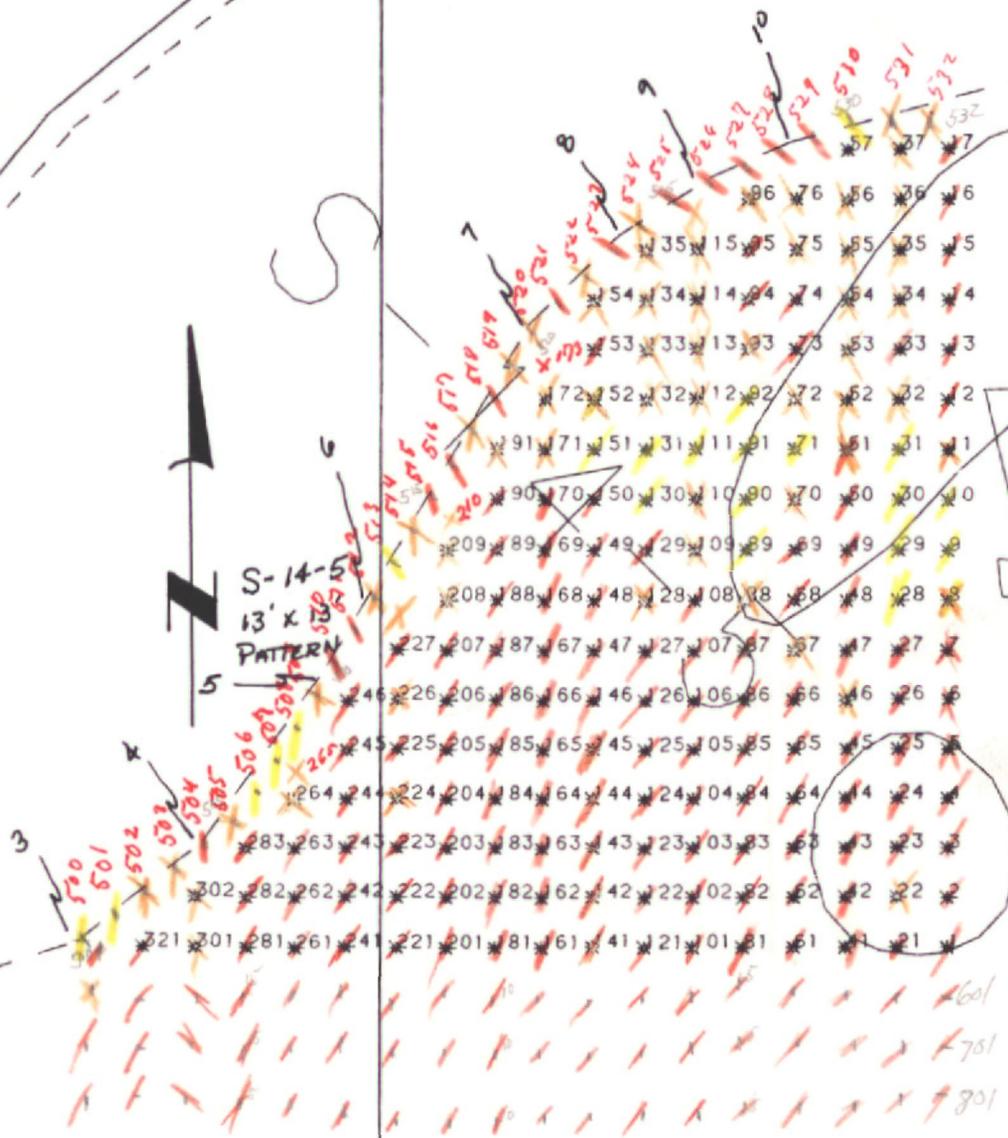
3 ok

S14	5	605	3	0.040	ERR
S14	5	606	3	0.033	ERR
S14	5	607	3	0.068	ERR
S14	5	608	3	0.022	ERR
S14	5	609	3	0.083	ERR
S14	5	610	3	0.066	ERR
S14	5	611	3	0.128	ERR
S14	5	612	3	0.065	ERR
S14	5	613	3	0.105	ERR
S14	5	614	3	0.045	ERR
S14	5	615	3	0.064	ERR
S14	5	616	3	0.012	ERR
S14	5	617	3	0.008	ERR
S14	5	618	3-2	0.017	ERR
S14	5	701	3	0.019	ERR
S14	5	702	3	0.019	ERR
S14	5	703	3	0.006	ERR
S14	5	704	3	0.025	ERR
S14	5	705	3	0.014	ERR
S14	5	706	3	0.022	ERR
S14	5	707	3	0.065	ERR
S14	5	708	3	0.036	ERR
S14	5	709	3	0.063	ERR
S14	5	710	3	0.069	ERR
S14	5	711	3	0.073	ERR
S14	5	712	3	0.047	ERR
S14	5	713	3	0.104	ERR
S14	5	714	3	0.062	ERR
S14	5	715	3	0.016	ERR
S14	5	716	3	0.029	ERR
S14	5	717	3	0.037	ERR
S14	5	718	3	0.017	ERR
S14	5	801	3	0.030	ERR
S14	5	802	3	0.011	ERR
S14	5	803	3	0.013	ERR
S14	5	804	3	0.011	ERR
S14	5	805	3	0.017	ERR
S14	5	806	3	0.045	ERR
S14	5	807	3	0.020	ERR
S14	5	808	3	0.023	ERR
S14	5	809	3	0.070	ERR
S14	5	810	3	0.033	ERR
S14	5	811	3	0.031	ERR
S14	5	812	3	0.039	ERR
S14	5	813	3	0.041	ERR
S14	5	814	3	0.026	ERR
S14	5	815	3	0.011	ERR
S14	5	816	3	0.010	ERR
S14	5	817	3	0.019	ERR
S14	5	818	3	0.010	ERR

ORE - TYPE



S-14-5
13' x 13'
PATTERN



5000.
0000.

601
701
801

4-12-90

72

4-16-90

22

4-17-90

33

4-18-90

69

4-19-90

70

4-19-90

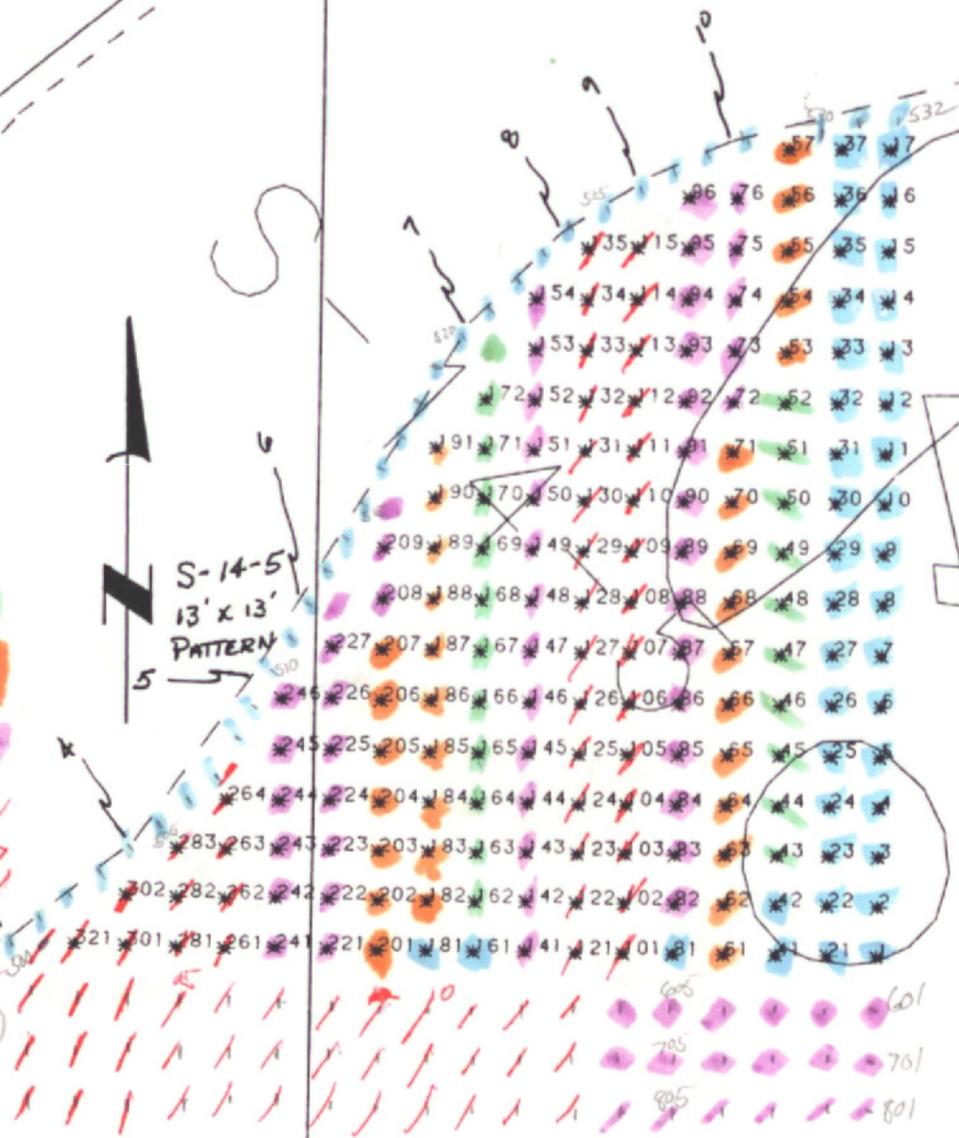
71

274



S-14-5
13' x 13'
PATTERN

5



SAMPLE PICK-UP

45000
27000

500-532

33
34
4
71

Pit-Bench-Pattern #

5-14-5

BLAST HOLE

DATE:

4/20/90

Submittal Date

4/19/90 1:15 p.m.

Hot NaCN Shake

and

NAME:

W.D.

FIRE DETERMINATIONS

#3:15p

	FIRE	NaCN		FIRE	NaCN
SAMPLE	Au.	Au.	SAMPLE	Au.	Au.
1. 301		.013	25. Standard ✓		.015
2. 302		.016	26. 715		.016
3. 607-1		.065	27. 716		.029
4. 607-2		.070	28. 807		.020
5. 608		.022	29. 808		.023
6. 609		.083	30. 809		.070
7. 610		.066	31. 810		.033
8. Standard ✓		.015	32. 811		.031
9. 611		.128	33.		
10. 612		.065	34.		
11. 613		.105	35. 812		.039
12. 614		.045	36. 813		.041
13. 615		.064	37. 814		.026
14. 616		.012	38. 815		.011
15. 707		.065	39. 816		.010
16.			40. V6		.028
17.			41. 321		.015
18. 708		.036	42. Standard ✓		.015
19. 709		.063	43. 341		.017
20. 710		.069	44. 617		.008
21. 711		.073	45. 618		.017
22. 712		.047	46. 717		.037
23. 713		.104	47. 718		.017
24. 714		.062	48. 817		.019

0.68

818

std ✓

.010
.014

BROWN MINING CORPORATION
Oilt Edge Project

Pit-Bench-Pattern #

5-14-5

BLAST HOLE

DATE: 4/19

Submittal Date

4/18/90 1:15p (cont.)

Hot NaCN Shake
and
FIRE DETERMINATIONS

NAME: KW

	FIRE	NaCN		FIRE	NaCN
	SAMPLE	Au.		SAMPLE	Au.
1.	222		25.	Standard ✓	.015
2.	223		26.	✓ 6	.027
3.	224		27.	703	.006
4.	225		28.	704	.025
5.	226		29.	705	.014
6.	227		30.	706	.022
7.	228		31.	801	.030
8.	Standard ✓	.015	32.	802	.011
9.	241		33.		
10.	242		34.		
11.	243		35.	803	.013
12.	244		36.	804	.011
13.	245		37.	805	.017
14.	246		38.	806-1	.043
15.	601		39.	806-2	.046
16.			40.		
17.			41.		
18.	602		42.	Standard ✓	.015
19.	603		43.		
20.	604		44.		
21.	605		45.		
22.	606		46.		
23.	701		47.		
24.	702		48.		

.045

BROWN MINING CORPORATION
Gilt Edge Project

Pit-Bench-Pattern #

5-14-5

Submittal Date

4/19/90 1:15p

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE:

4/20/90

NAME:

WD WD

	FIRE	NaCN		FIRE	NaCN
	SAMPLE	Au.	Au.	SAMPLE	Au.
1.	✓6		.027	25. Standard ✓	.015
2.	101		.021	26. 126	.012
3.	102		.031	27. 127	.011
4.	103		.023	28. 128	.002
5.	104		.034	29. 129	.006
6.	105		.048	30. 130	.004
7.	106		.032	31. 131	.005
8.	Standard ✓		.014	32. 132	.003
9.	107		.014	33.	
10.	108		.002	34.	
11.	109		.007	35. 133	.007
12.	110		.006	36. 134	.004
13.	111		.004	37. 135	.006
14.	112		.003	38. 261	.038
15.	113		.002	39. 262	.024
16.				40. 263	.009
17.				41. 264	.006
18.	114		.005	42. Standard ✓	.015
19.	115		.026	43. 265-1	.008
20.	121		.037	44. *265-2	.008
21.	122		.054	45. 281	.013
22.	123		.063	46. 282	.042
23.	124		.037	47. 283	.006
24.	125		.014	48. Standard ✓	.014

BROWN MINING CORPORATION
Oilt Edge Project

Pit-Bench-Pattern #

5-14-5

BLAST HOLE

DATE:

4/19

Submittal Date

4/18/90 115P

Hot NaCN Shake

and

FIRE DETERMINATIONS

NAME:

W

	FIRE	NaCN		FIRE	NaCN
	SAMPLE	Au.		SAMPLE	Au.
1.	72		25.	Standard ✓	.014
2.	73		26.	141	.058
3.	74		27.	142	.124
4.	75		28.	143	.156
5.	76		29.	144	.044
6.	82		30.	145	.035
7.	83		31.	✓6	.027
8.	Standard ✓		32.	146	.014
9.	84		33.		
10.	85		34.		
11.	86		35.	147	.015
12.	87		36.	148	.009
13.	88		37.	149	.008
14.	89		38.	150	.005
15.	90		39.	151	.006
16.			40.	152	.005
17.			41.	153	.006
18.	91		42.	Standard ✓	.015
19.	92		43.	154	.004
20.	93		44.	208	.002
21.	94		45.	209	.003
22.	95		46.	210	.006
23.	96-1		47.	221	.047
24.	96-2		48.	Std ✓	.014

ok

Pit-Bench-Pattern #
S-145

BLAST HOLE

DATE: 7/16/90

Submittal Date
4/12/90 11:50 AM

Hot NaCN Shake
and
FIRE DETERMINATIONS

NAME: ku

	FIRE		NaCN		FIRE		NaCN	
	SAMPLE	Au.	Au.		SAMPLE	Au.	Au.	
1.	181		.077	25.	Standard ✓		.014	
2.	500		.004	26.	520		.004	
3.	501		.006	27.	521		.005	
4.	502		.004	28.	522		.004	
5.	503		.010	29.	523		.005	
6.	504		.003	30.	524		.006	
7.	505		.004	31.	525		.003	
8.	Standard ✓		.015	32.	526		.006	
9.	506		.006	33.				
10.	507		.026	34.				
11.	508		.003	35.	527		.012	
12.	509		.001	36.	528		.005	
13.	510		.001	37.	529		.002	
14.	511		7W	38.	530		.001	
15.	512		.003	39.	531-1		.002	
16.				40.	531-2		.004	
17.				41.	532		.003	
18.	513		.002	42.	Standard ✓		.014	
19.	514		.003	43.	V6		.027	
20.	515		.005	44.				
21.	516		.007	45.				
22.	517		.004	46.				
23.	518		.006	47.				
24.	519		.003	48.				

.003

Pit-Bench-Pattern #

5-14-5

BLAST HOLE

DATE: 4-17-90

Submittal Date

4-16-90

9:45

Hot NaCN Shake
and

NAME: ~~VD~~ VD

FIRE DETERMINATIONS

FIRE		NaCN		FIRE		NaCN	
SAMPLE	Au.	Au.		SAMPLE	Au.	Au.	
1.	43		.058	25.	Standard ✓	.014	
2.	upwr		.031	26.	171	.004	
3.	44		.041	27.	172	.003	
4.	45		.072	28.	173	.003	
5.	46		.046	29.	Standard ✓	.014	
6.	47		.036	30.			
7.	48		.017	31.			
8.	Standard ✓		.015	32.			
9.	49		.015	33.			
10.	50		.015	34.			
11.	51		.011	35.			
12.	52		.012	36.			
13.	162		.101	37.			
14.	163		.011	38.			
15.	164		.099	39.			
16.				40.			
17.				41.			
18.	165		.029	42.	Standard ✓		
19.	166-1		.010	43.			
20.	166-2		.010	44.			
21.	167		.005	45.			
22.	168		.004	46.			
23.	169		.003	47.			
24.	170		.004	48.			

BROWN MINING CORPORATION
0111 Edge Project

Pit-Bench-Pattern #

5-14-5

Submission Date

4/12/90 1:15P

BLAST HOLE

Hot NaCN Shake

and

FIRE DETERMINATIONS

DATE: 4/16/90

NAME: KW

FIRE		NaCN		FIRE		NaCN	
SAMPLE	Au.	Au.		SAMPLE	Au.	Au.	
1.	1		.015	25.	Standard ✓	.014	
2.	2		.013	26.	23	.032	
3.	3		.027	27.	24	.046	
4.	4		.068	28.	25	.091	
5.	5		.124	29.	26	.051	
6.	6		.050	30.	27	.145	
7.	7		.100	31.	28	.031	
8.	Standard ✓		.014	32.	29	.022	
9.	8		.100	33.			
10.	✓6		.027	34.			
11.	9		.063	35.	30	.042	
12.	10		.022	36.	31	.029	
13.	11		.036	37.	32	.018	
14.	12		.045	38.	33	.009	
15.	13		.009	39.	34	.008	
16.				40.	35	.010	
17.				41.	36	.008	
18.	14		.015	42.	Standard ✓	.015	
19.	15-1		.006	43.	37	.007	
20.	15-2		.006	44.	41	.027	
21.	16		.019	45.	42	.038	
22.	17		.011	46.	81	.011	
23.	21		.031	47.	161	.033	
24.	22		.033	48.	SHV	.014	

Pit-Bench-Pattern #

5-14-5

Submittal Date

4-17-90

BLAST HOLE

Hot NaCN Shake

and

FIRE DETERMINATIONS

DATE: 4-18-90

NAME: BA-20

	FIRE	NaCN		FIRE	NaCN
	SAMPLE	Au.		SAMPLE	Au.
1.	53	.007	25.	Standard ✓	.015
2.	54	.015	26.	185	.021
3.	55	.007	27.	186	.007
4.	56	.005	28.	187	.009
5.	57	.003	29.	188	.009
6.	61	.017	30.	189	.005
7.	✓ pulp	.026	31.	190	.005
8.	Standard ✓	.015	32.	191	.005
9.	62	.022	33.		
10.	63	.033	34.		
11.	64	.033	35.	201	.047
12.	65	.024	36.	202	.023
13.	66	.045	37.	203	.110
14.	67-A	.016	38.	204	.007
15.	67-B	.017	39.	205	.080
16.			40.	206	.024
17.			41.	207	.007
18.	68	.017	42.	Standard ✓	.014
19.	69	.024			
20.	70	.023			
21.	71	.008	45.		
22.	182	.159	46.		
23.	183	.017	47.		
24.	184	.062	48.		